

Model Order Reduction for Design with Signal Integrity

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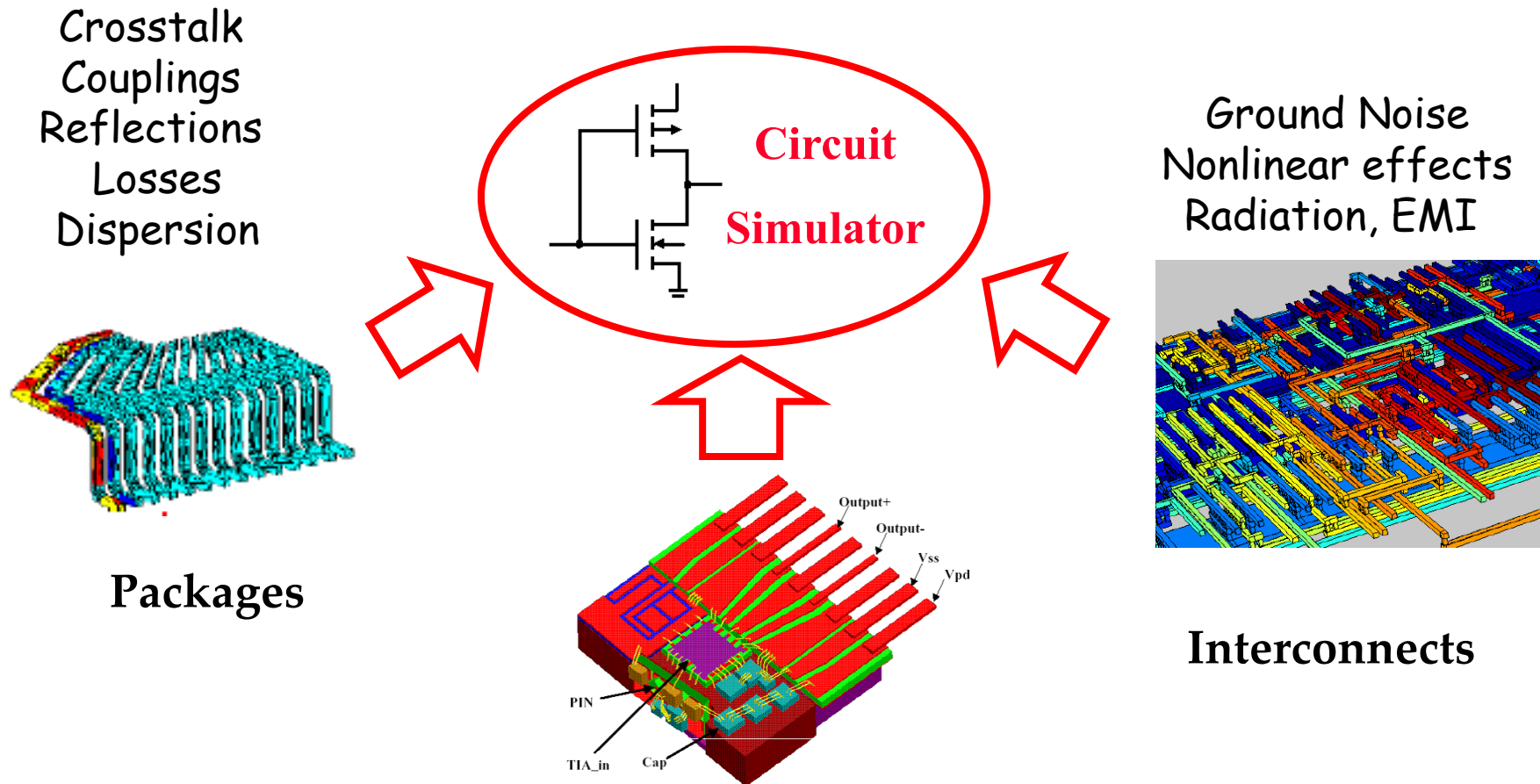
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IBIS Talk

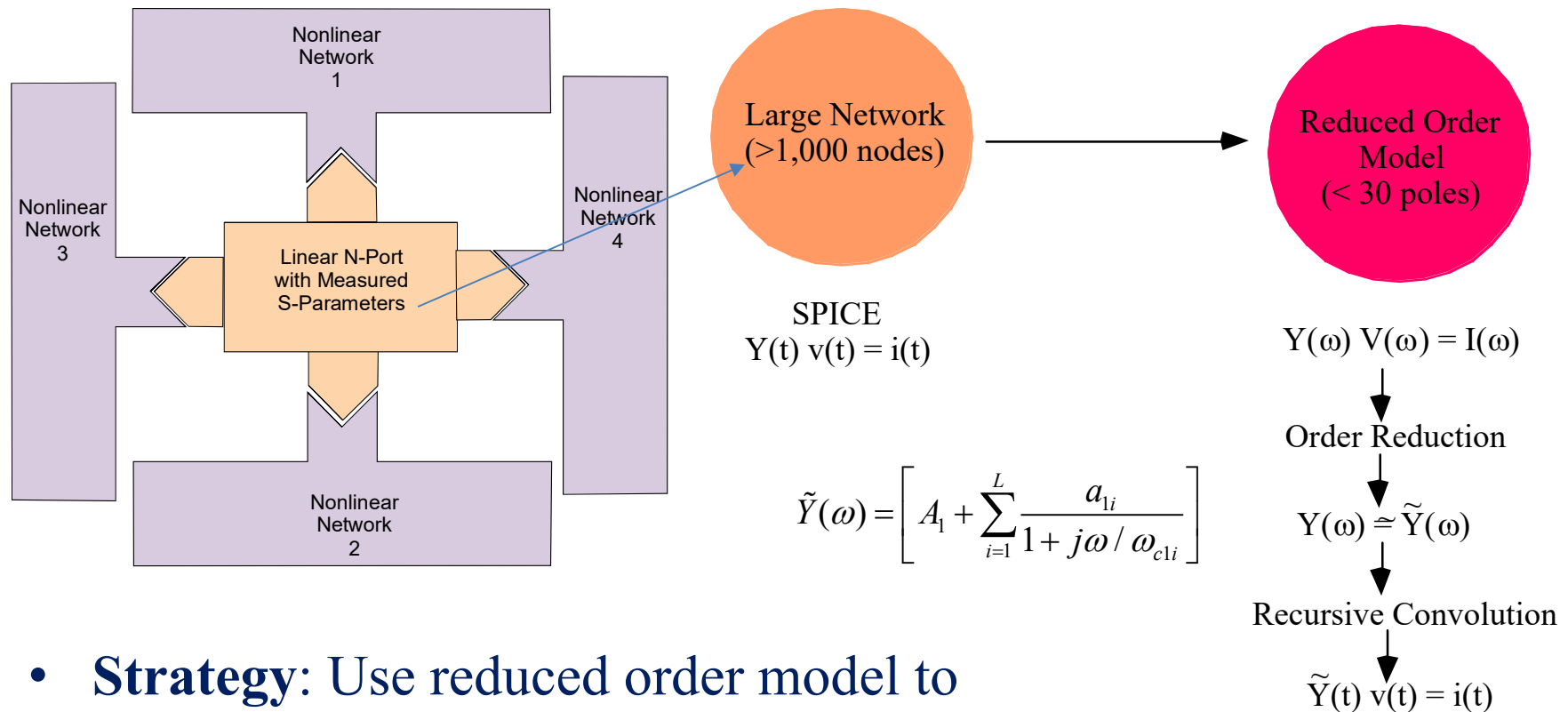
January 26, 2022



Interconnect Structures



Model-Order Reduction

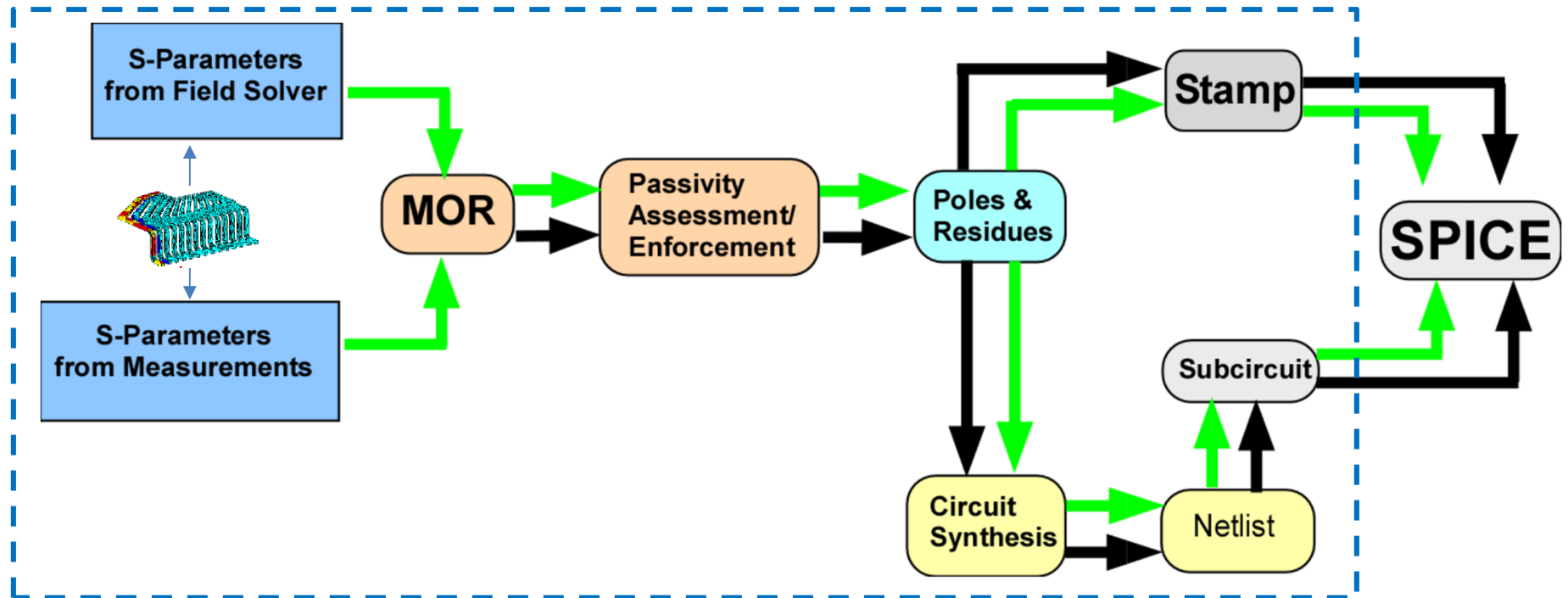


- **Strategy:** Use reduced order model to minimize computation time.

$$\tilde{Y}(\omega) \ll Y(\omega)$$



Model-Order Reduction

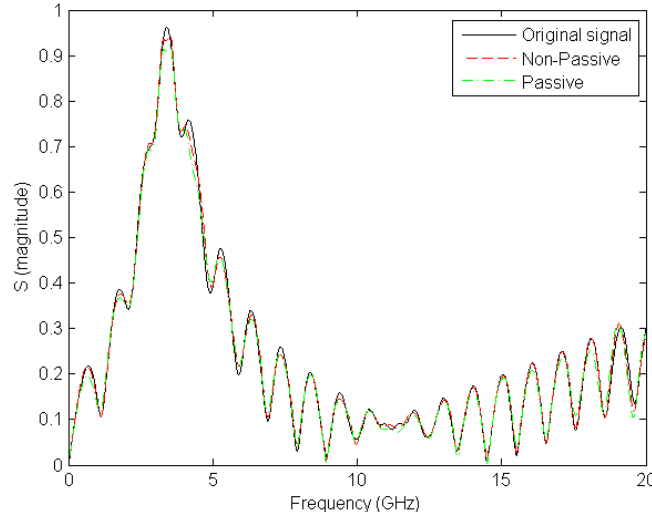


- **Objective:** Incorporate frequency dependence into time-domain simulator
- **Approaches:** 1) Direct integration of code into SPICE – 2) Generation of SPICE-compatible netlist



Model-Order Reduction

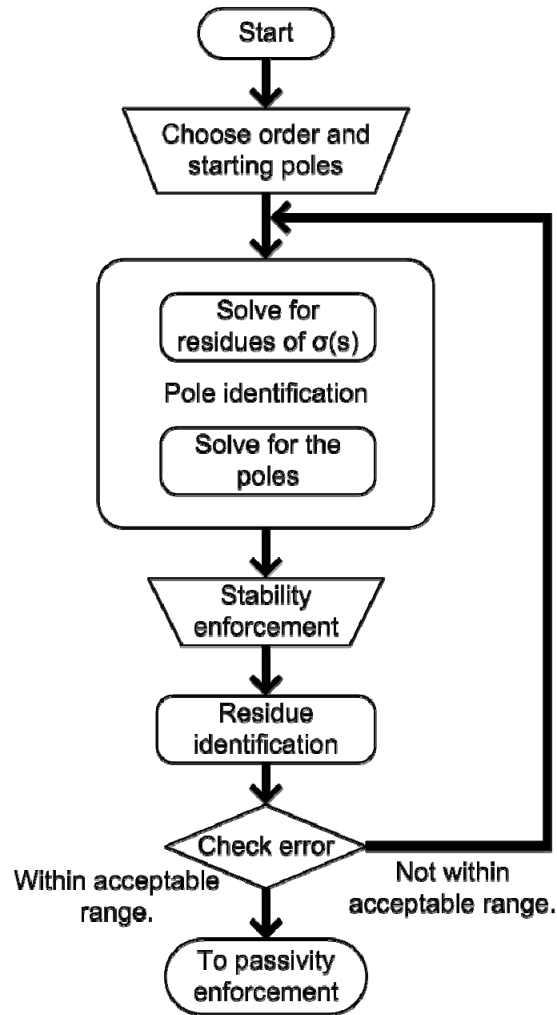
- Start with S parameters from field solver
- Use vector fitting to get poles & residues
- Perform assessment via Hamiltonian
- Enforcement: Residue Perturbation Method
- Simulation: Recursive convolution → **Fast**



Number of Ports	Order	CPU-Time
4-Port	20	1.7 secs
6-port	32	3.69 secs
10-port	34	8.84 secs
20-port	34	33 secs
40	50	142 secs
80	12	255 secs



MOR via Vector Fitting



- Rational function approximation:

$$f(s) \approx \sum_{n=1}^N \frac{c_n}{s - a_n} + d + sh$$

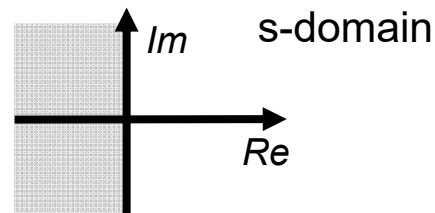
- Introduce an unknown function $\sigma(s)$ that satisfies:

$$\begin{bmatrix} \sigma(s)f(s) \\ \sigma(s) \end{bmatrix} \approx \begin{bmatrix} \sum_{n=1}^N \frac{c_n}{s - \tilde{a}_n} + d + sh \\ \sum_{n=1}^N \frac{\tilde{c}_n}{s - \tilde{a}_n} + 1 \end{bmatrix}$$

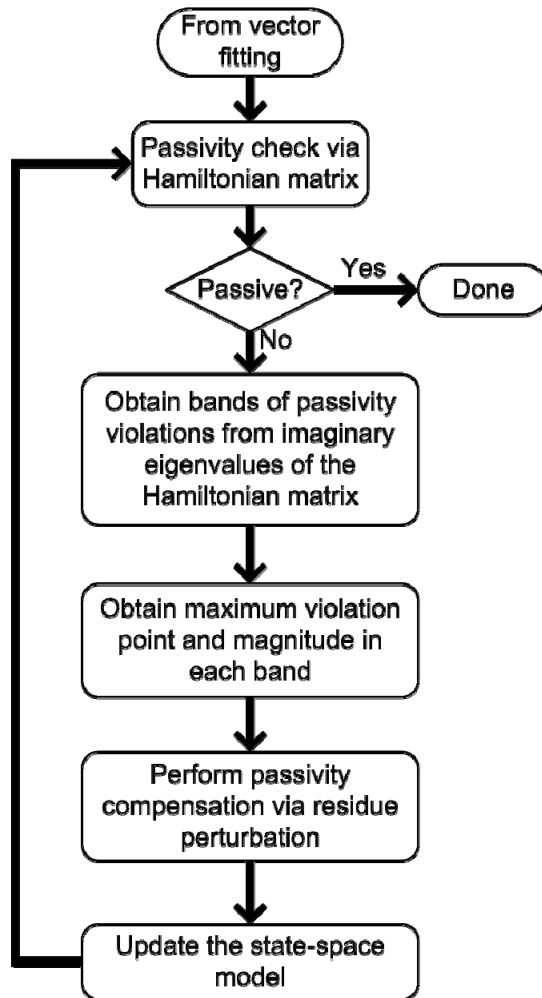
- Poles of $f(s)$
= zeros of $\sigma(s)$:

$$f(s) \approx \frac{\sum_{n=1}^N \frac{c_n}{s - \tilde{a}_n} + d + sh}{\sum_{n=1}^N \frac{\tilde{c}_n}{s - \tilde{a}_n} + 1} = \frac{\prod_{n=1}^{N+1} (s - z_n)}{\prod_{n=1}^N (s - \tilde{z}_n)}$$

- Flip unstable poles into the left half plane.



Passivity Enforcement



- State-space form:

$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

- Hamiltonian matrix:

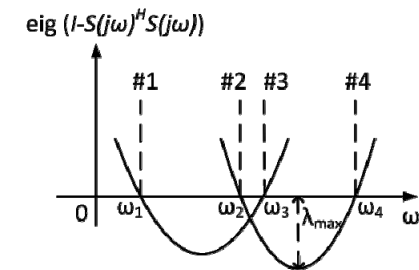
$$M = \begin{bmatrix} A + BKD^T C & BKB^T \\ -C^T L C & -A^T - C^T DKB^T \end{bmatrix}$$

$$K = (I - D^T D)^{-1} \quad L = (I - DD^T)^{-1}$$

- Passive if M has no imaginary eigenvalues.

- Sweep:

$$\text{eig}(I - S(j\omega)^H S(j\omega))$$



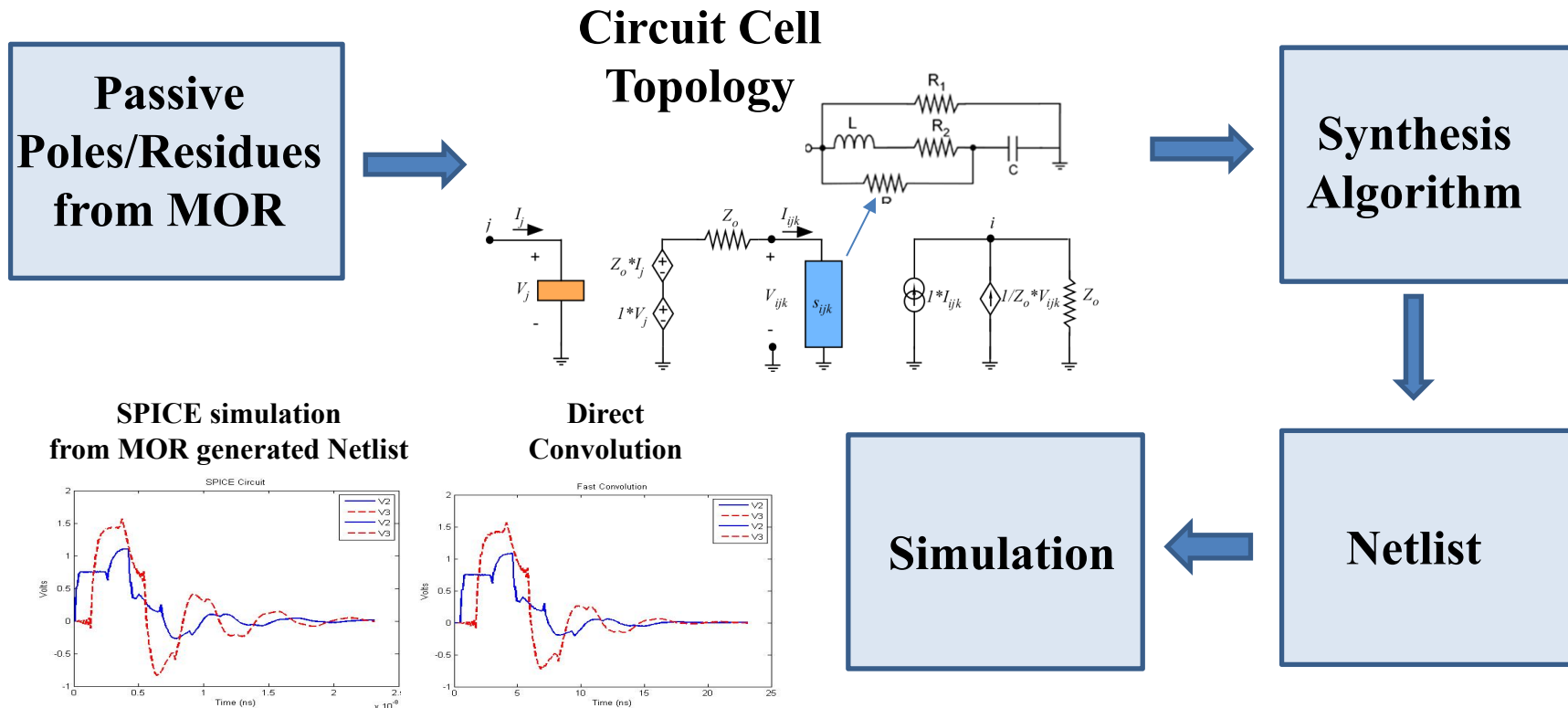
- Quadratic programming:

– Minimize (change in response) subject to (passivity compensation).

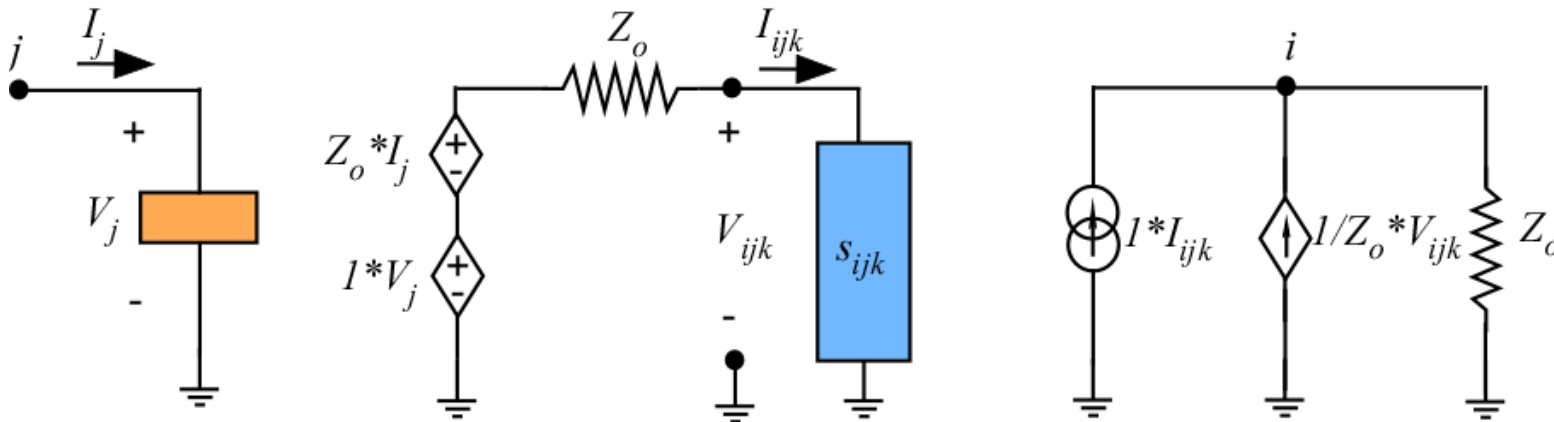
$$\min(\text{vec}(\Delta C)^T H \text{vec}(\Delta C)) \quad \text{subject to} \quad \Delta \lambda = G \cdot \text{vec}(\Delta C).$$

SPICE Netlist Synthesis

- Goal is to generate (using pole/residue information) a circuit netlist that will exhibit the same (frequency-dependent) behavior as that of the S-parameters of connector under study



S-Parameter Circuit Synthesis



$$A_i(\omega) = \frac{1}{2} [V_i(\omega) + Z_o I_i(\omega)]$$

$$B_i(\omega) = \frac{1}{2} [V_i(\omega) - Z_o I_i(\omega)]$$

Need equivalent circuit for S_{ijk}

Strategy

For a given circuit, a relationship between the input admittance $Y_{ijk}(s)$ of the circuit and the associated one-port S-parameter representation $S_{ijk}(s)$ can be described by

$$S_{ijk}(s) = \frac{Y_o - Y_{ijk}(s)}{Y_o + Y_{ijk}(s)} \quad Y_{ijk}(s) = Y_o \frac{1 - S_{ijk}(s)}{1 + S_{ijk}(s)}$$

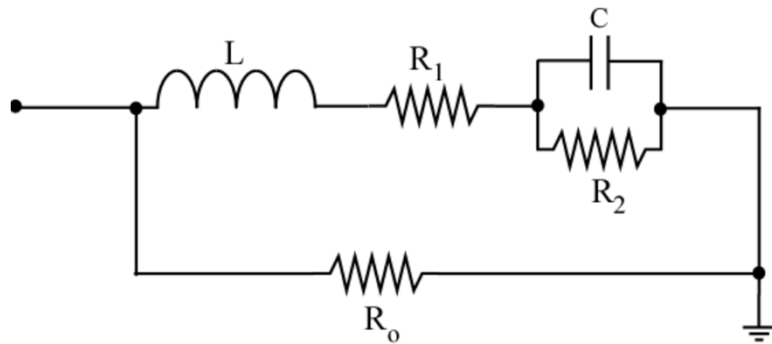
Y_o is the reference admittance



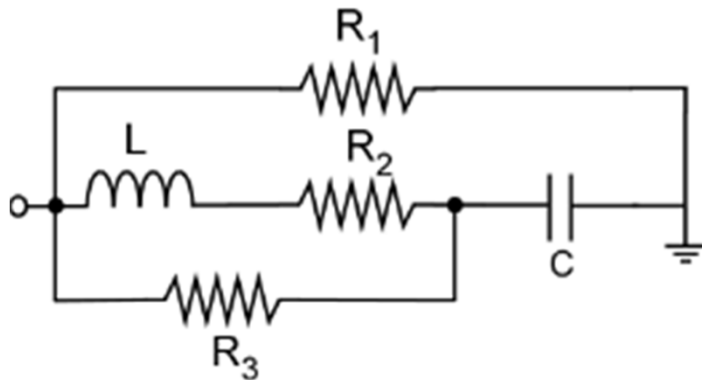
Realization – Complex Poles

There are several circuit topologies that will work

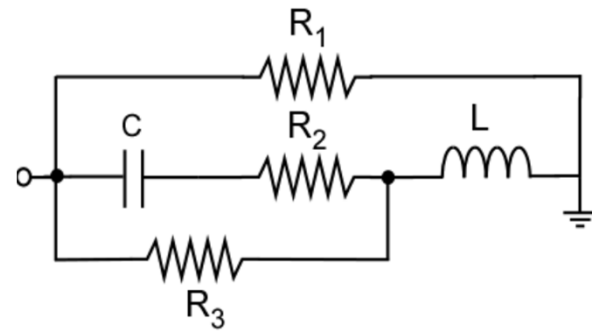
Model 1



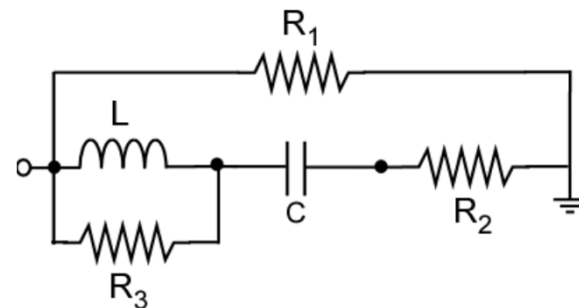
Model 9



Model 8



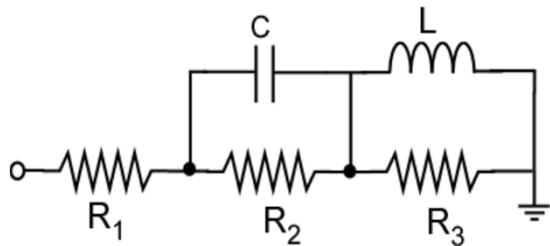
Model 10



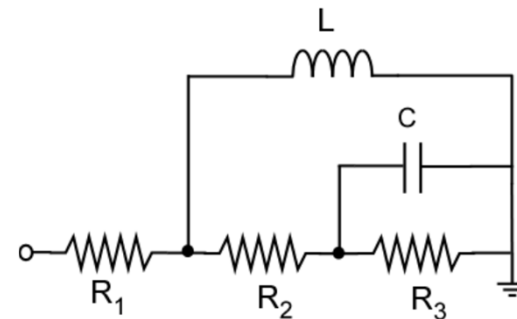
Realization – Complex Poles

More circuit topologies that will work

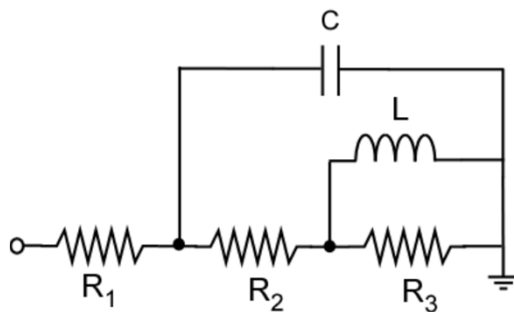
Model 11



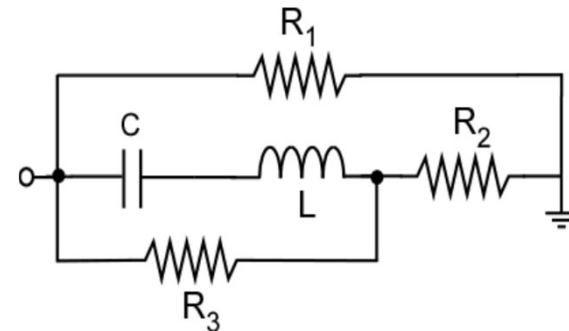
Model 12



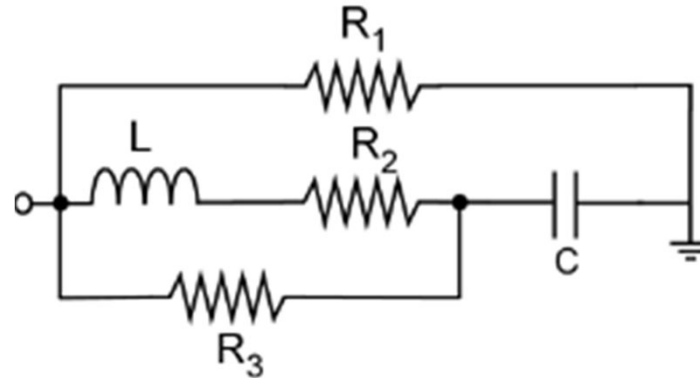
Model 13



Model D



Complex Poles – Model 9



$$R_1 = \frac{F}{BH}$$

$$C = \frac{(-BD + AF)H}{F^2}$$

$$R_2 = \frac{(-BD^2 + BF + ADF - F^2)}{(B^2 - ABD + BD^2 + A^2F - 2BF - ADF + F^2)H}$$

$$R_3 = \frac{F}{(-B + F)H}$$

$$L = \frac{-BD + AF}{(B^2 - ABD + BD^2 + A^2F - 2BF - ADF + F^2)H}$$

Netlist from Poles & Residues

```
*Myckt 2-port S-parameter circuit model
* 14 -pole approximation

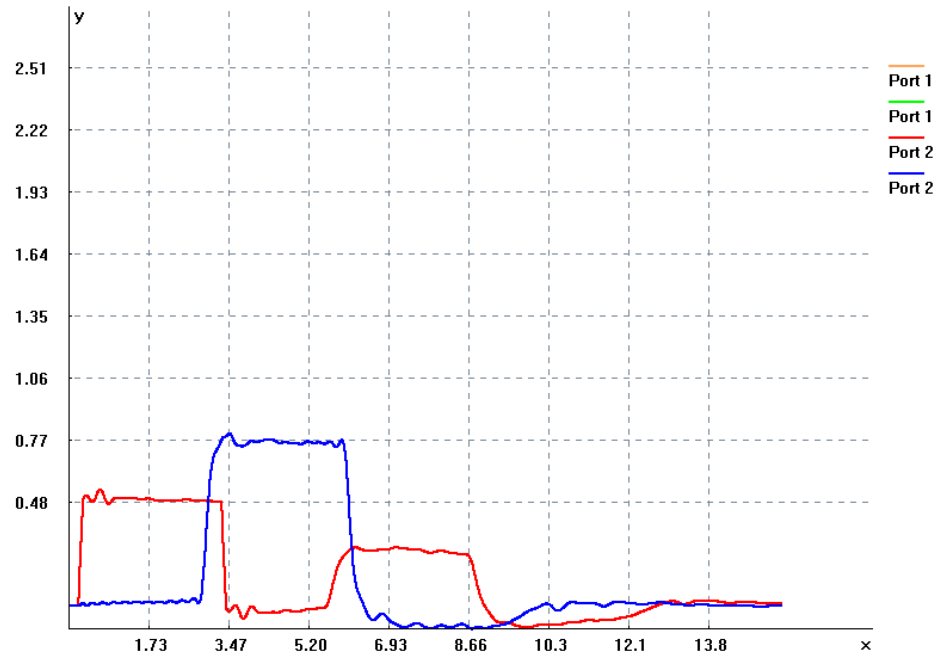
.subckt Myckt 42000 56000
vsens42001 42000 42001 0.0
vsens56001 56000 56001 0.0

*subcircuit for s[1][1]
*complex residue-pole pairs for S[1][1] at k= 1 -> 1st pole: -4.8961e+00 3.6506e+01 residue: 2.1006e-01 -2.8971e-01
*
-> 2nd pole: -4.8961e+00 -3.6506e+01 residue: 2.1006e-01 2.8971e-01

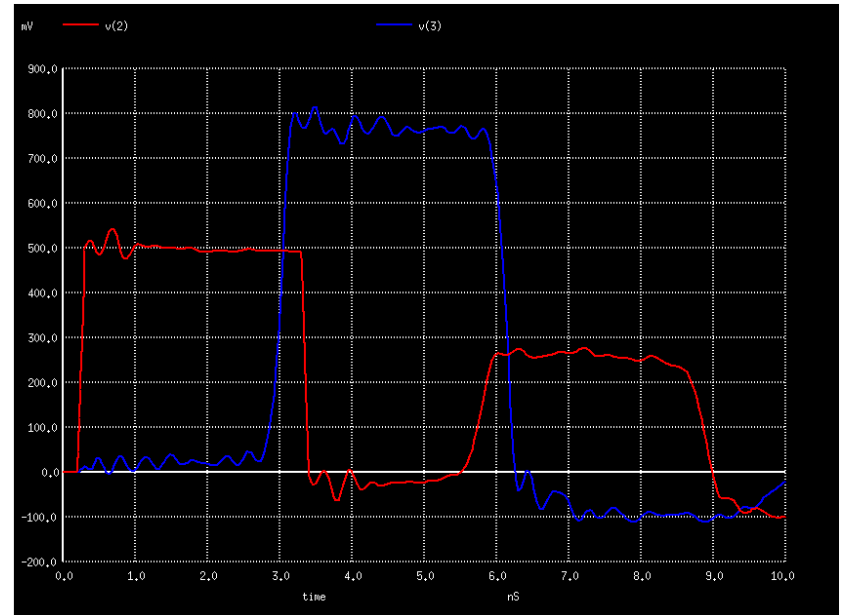
*circuit type = 9
elc1 1 0 42001 0 1.0
hc2 2 1 vsens42001 50.0
rtersc3 2 3 50.0
vp4 3 4 0.0
r1cd5 4 0 5.17406e+01
l1cd5 4 5 -1.25500e-08
r2cd6 5 6 -1.30103e+03
c1cd6 6 0 -7.19920e-15
r3cd6 4 6 1.48633e+03
*complex residue-pole pairs for S[1][1] at k= 2 -> 1st pole: -1.3039e+00 2.7679e+01 residue: -4.3856e-01 -1.9087e+00
*
-> 2nd pole: -1.3039e+00 -2.7679e+01 residue: -4.3856e-01 1.9087e+00

rtersc9 8 9 50.0
:
:
gs196 0 56001 196 0 0.020
rnort42001 42001 0 5.00000e+01
rnort56001 56001 0 5.00000e+01
.ends Myckt
*main circuit
rgen 1 2 50.0
x1 2 3 Myckt
vin 1 0 pulse (0 1 0.20000ns 0.10000ns 0.10000ns 2.00000ns 6.00000ns)
rport2 3 0 50000.0000000
.tran 0.00039ns 7.00000ns
.end
```

2-Port Network



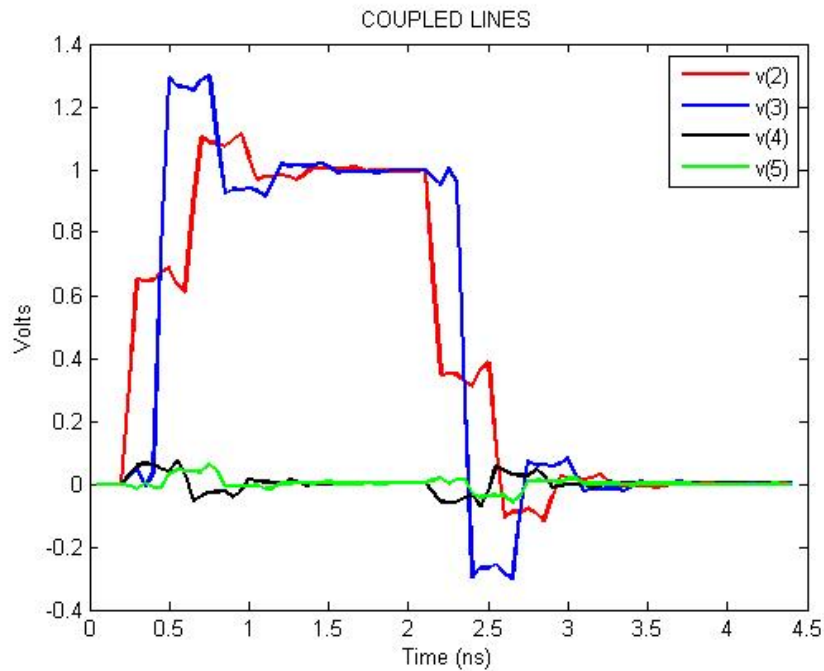
Recursive convolution



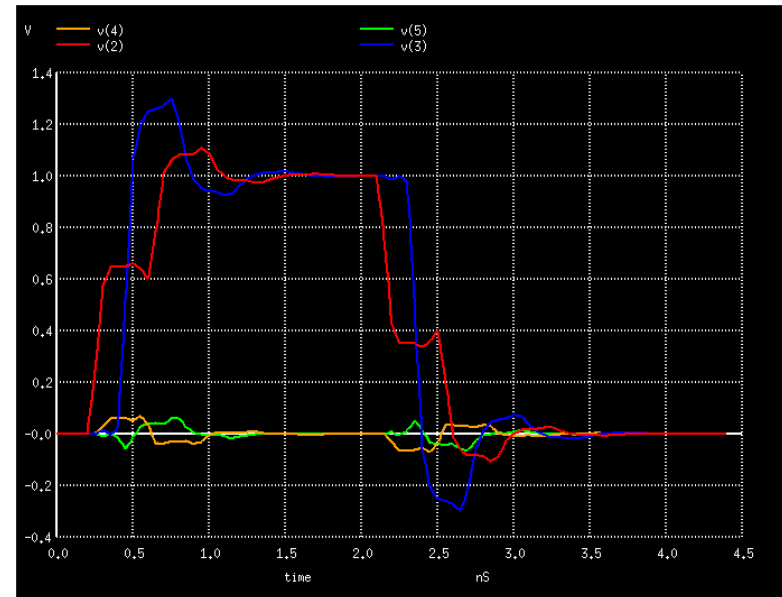
SPICE realization

4-Port Network

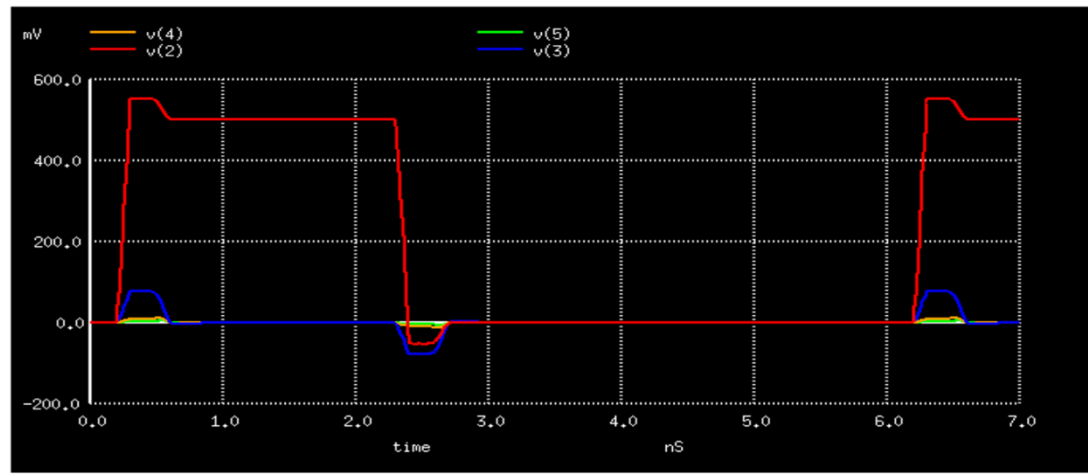
Direct



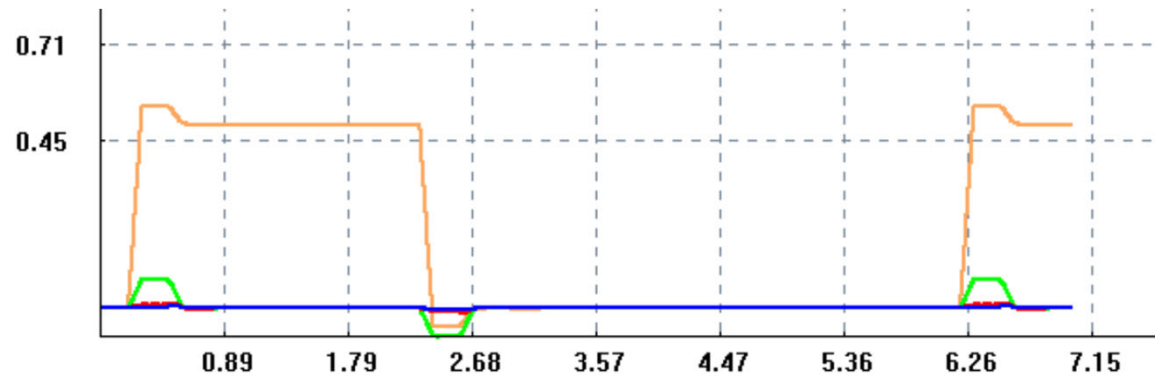
SPICE simulation Using generated netlist (Method 2)



8-Port Network

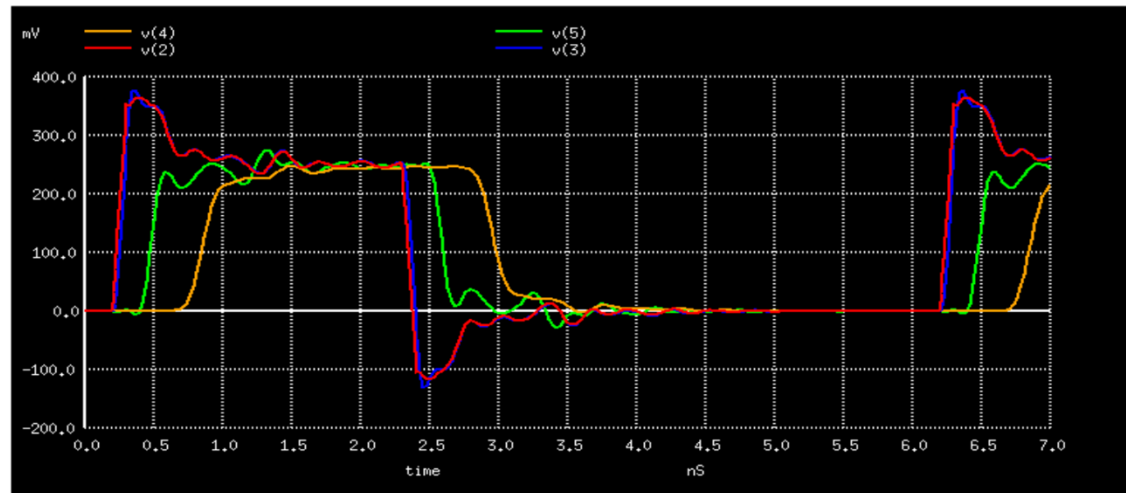


SPICE
simulation
Using
generated
netlist

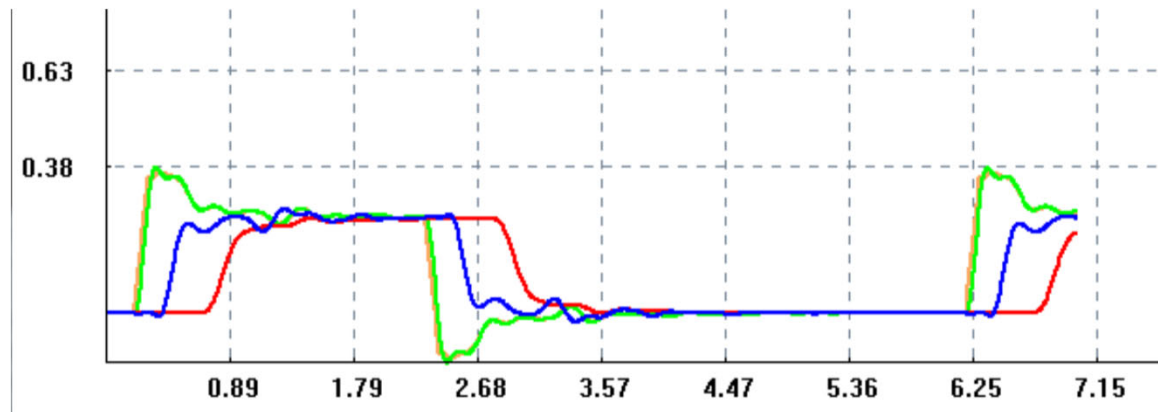


Direct

10-Port Network

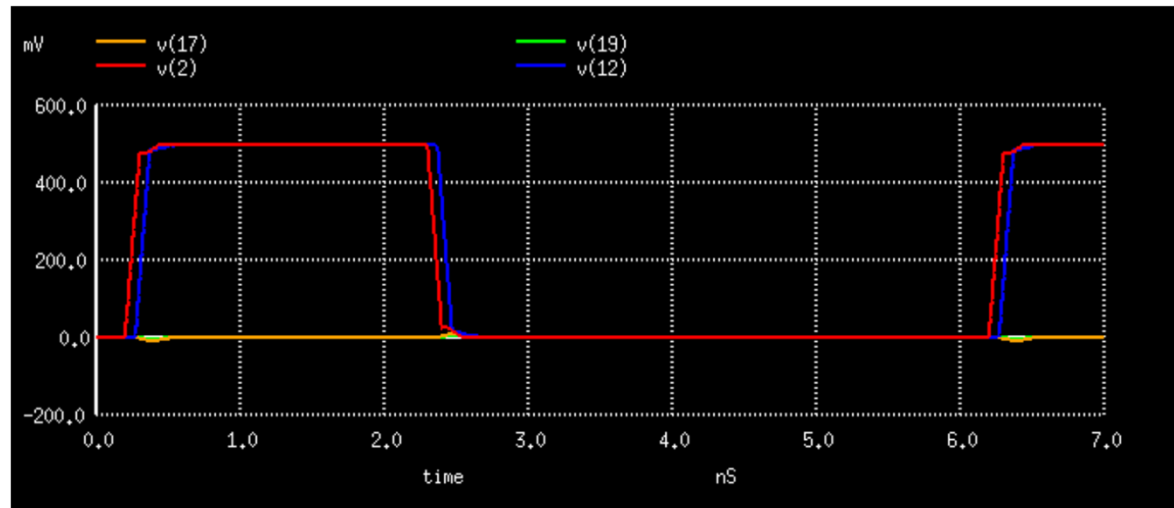


SPICE
simulation
Using
generated
netlist

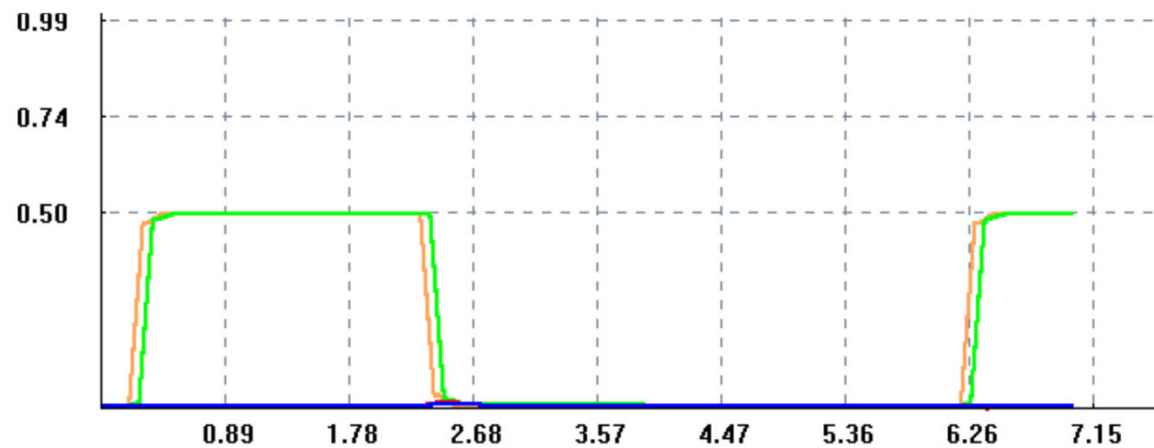


Direct

20-Port Network



SPICE
simulation
Using
generated
netlist



Direct

Conclusion

- S-parameter based SPICE circuits are robust
- Several topologies can be used for complex poles
- 20-port networks have been successfully tested
- Good agreement with direct simulations

